

The extraction and separation of Copper(II) from its aqueous solutions, by using swelled crown ether (PDB18C6)

/ / /

(NJC)

(2006 /11 / 15) (2006/ 4 / 2)

(II)

:

PDB18C6

:

(E%=93.5)

(pH=10) (II)

(HNO₃ , H₂SO₄ , HCl)

(II)

.KOH

(0.01)

(E%=98)

(60)

(E%=64.2) (II)

(20±1C°)

(40%V/V)

(KCl , NaCl)

(II)

PDB18C6

(II)

(F⁻ , I⁻ , Cl⁻ , Br⁻)

(Rb⁺ , K⁺ , Na⁺ , Li⁺ , Mg⁺² , Ni⁺² , Cd⁺² , Ca⁺² , Sr⁺² , Ba⁺²)

(II)

ΔHex

ΔSex

ΔGex

(II)

		(II)	(II)	
		KOH	(2.0)	(PDB18C6)
			(10)	Pd(II)
(1)	(10)		HCl	(1.0)
				/

Abstract

This study included the extraction and separation of Copper(II) from its aqueous solutions, by using swelled crown ether (PDB18C6), and included the following:

It was found that; the copper(II) is extracted when (pH=10), percentage extraction reached (E%=93.5).but Its extraction was impossible from the acidic media (HCl , H₂SO₄, HNO₃). The results also showed that the alkaline media was suitable for the extraction of copper(II), and the high percentage value for it's equal to (E%=98) was obtained at [0.01M] from KOH. It was found from experiments that the best shaking time was (60) minutes. Adding ethanol to aqueous phase (40%V/V) at(20±1C°) temperature gave the best extraction percentage for copper (II) (E%=64.2).

Percentage extraction of copper(II) from the salt media (KCl, NaCl) were low in comparison with the alkaline media. The selectivity of saturated solid polymer towards the extraction of copper(II) ions, in the present of the positive ion (Li⁺, Na⁺, K⁺, Rb⁺, Ba⁺², Sr⁺², Ca⁺², Cd⁺², Ni⁺², Mg⁺²) and the negative ions (F⁻, Br⁻, Cl⁻, I⁻), was also studied.

The effect of temperature and thermodynamics functions on the process of extraction of copper(II) ions was studied, and it appeared that the extraction enthalpy ΔH_{ex} , has a negative value in the case of copper, which means that the extraction process is exothermic and the free energy for extraction ΔG_{ex} showed negative value and the extraction entropy ΔS_{ex} showed positive value at all temperatures. Which means that the reaction is instantaneous.

The separation of copper from palladium ions was done on a chromatographic column filled with the substance (PDB18C6), which is treated previously with (2.0M) KOH solution, and by using the same solution as a mobile phase to elute Pd (II) first. The process was done on eight batches, and in each batch (10ml) was used from the mobile phase, while in the case of other eluted back the copper from column, (1.0M) of HCl was used for five batches, and in each batch (10ml) was used, and the speed of flow-rate for both ions was 1ml/min.

(II) ^[1] Townson

.95%

ACORGA M₅640

Timoore

(Cu⁺²)

(II) [2,3] Beniamin Lenarik

N,N-

dialkylpyridine-3-Carboxamides

(0.31 × 10⁻⁴ M)

(1-butyl

(II)

to 1-decyl)-4-methyl imidazol

[10,11]

Komiya

(Xylene,Toluene,

.Trichloromethane)

18-Crown-6

dichloromethane

KCl CuCl₂

[4,5]

Elzbieta

CuCl₂/18-Crown-

n-hexane

) 1-alkyl-1,24-triazoles

(X-ray)

6/KCl

(hexadecyl butyl =

(2-Ethyl-1-1hexanol)

KCl

Cyclohexane

arylalldoxime (p50)

.18C6

CuCl₂/15-

.Crown-5/NaCl

.Ketoxime

(II)

[6]

Saito

[12,13]

PDB18C8

(-)

Cu(II)

(Ion-pair-

thia Crown ethers

.association)

Cu(II)

.PDB18C6

Pd(II)

(TTCT)

.b

ab

(1

Double beam UV-Vis.
spectrophotometer, (Centra 5, Astral).

perchlorate

ab

(2

[7,8]

pH>4

Shaker, Wrist Action, Burvell
Corporation, PA, U.S.A.

[9]

Heekim

(3

hydroxamic acid

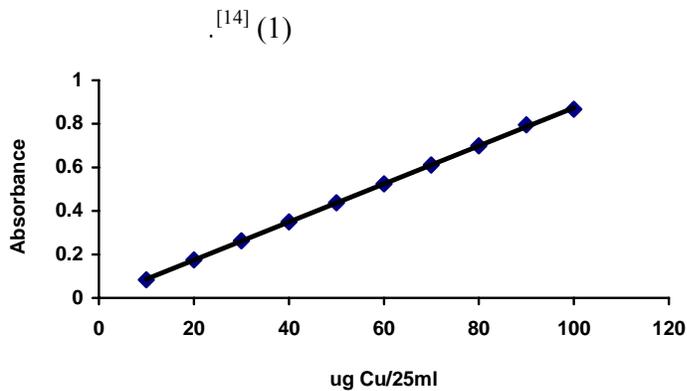
(II)

pH Meter 3320 JENWAY

15-Crown-5-ether

(Na- (0.1000) (4)
 (100) DDTC) Digital balance-Sartoris, (BP 3015-
 (8.5) pH Germany)
 (II) 2 (5)
 (II) 1-2 Water Bath, Gesellschaft fur
 Labortechnik Germany
 (II)
 ($6.35 \times 10^{-5} - 6.35 \times 10^{-6}$) 1

(100µg – 10µg)
 (25) Riedl- Dehean BDH Fluka
 (2) (100) (PDB18C6)
 (EDTA) (0.1) . Fluka %97.0
 (Potassium (20%) (2) 1-1
 Sodium Tartarate) (1mg) (II) -
 (~8.5) pH (0.3928) Cu/ml)
 (2)
 (CCl₄) (10) (Na-DDTC) (CuSO₄.5H₂O)
 H₂SO₄ (1)
 (100)
 (CCl₄) ($\lambda_{max} = 436nm$) -



(II) (1)

Least Square method

(r) correlation Coefficient = 0.9998

(a) Intercept = -0.0007157

(b) Slope = $13775.7 \text{ L.mol}^{-1} . \text{cm}^{-1}$

$$[\text{Cu}]\mu\text{g/ml} = \frac{[\text{Abs}] - \text{Intercept}}{\text{Slope}}$$

(II) 2-2

(II)

(100μg/ml)

[15] (Stripping)

(II)

(II)

(1)

(0.1)

(25)

(10)

(10)

(0.1)

[PDB18C6]

(II)

(60)

4-2

(II)

(II)

3-2

kd

(II)

[16,17]

E%

(1)

$$\frac{\text{.....}}{1} = D$$

$$D = kd$$

$$kd = \frac{C_{\text{org}}}{C_{\text{aq}}} \times \frac{V_{\text{ml}}}{W_{\text{g}}} \dots\dots\dots (2)$$

: () E%

$$E\% = \frac{C_{\text{org}}}{C_0} \times 100 \dots\dots\dots (3)$$

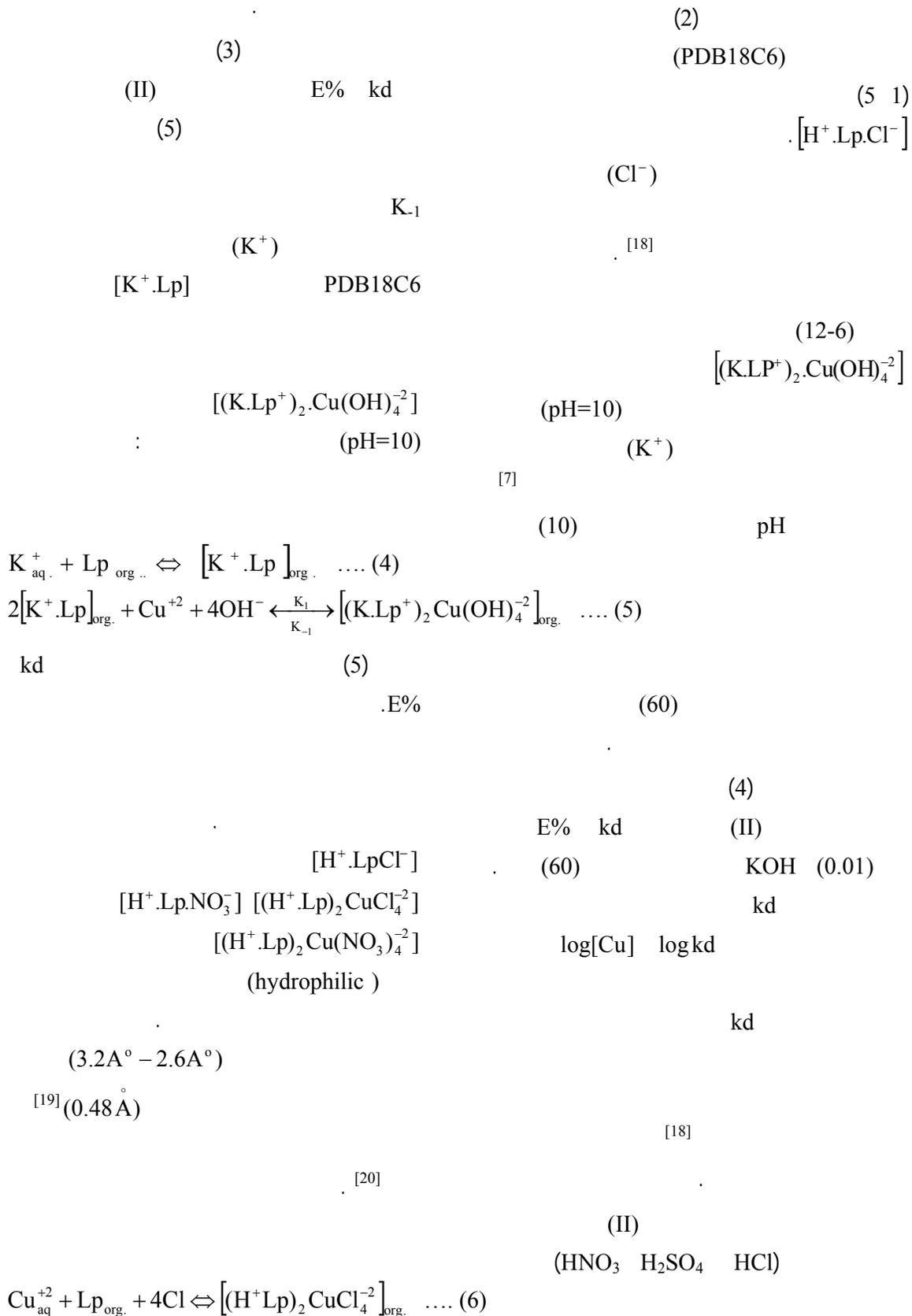
(C₀) .

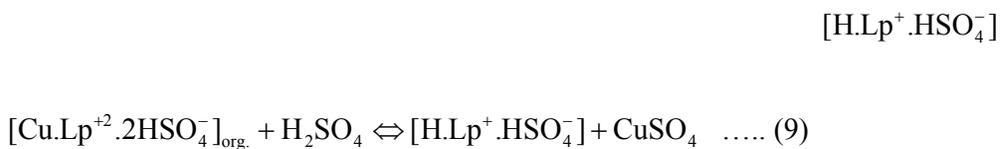
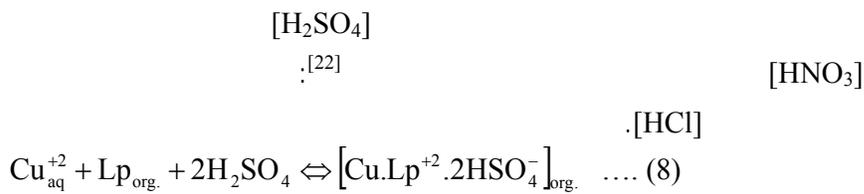
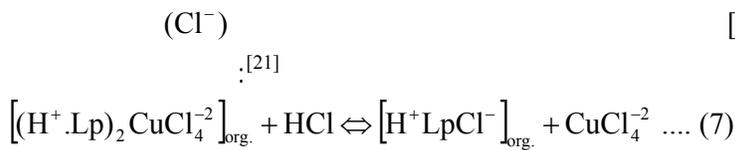
(C_{aq}) .

(C_{org}) .

= (W_g) .

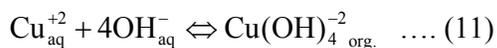
(V_{ml}) .





(II)

:



[23]

(hydrophilic)

(K⁺, Na⁺) M⁺
PDB18C6 Lp

(6)

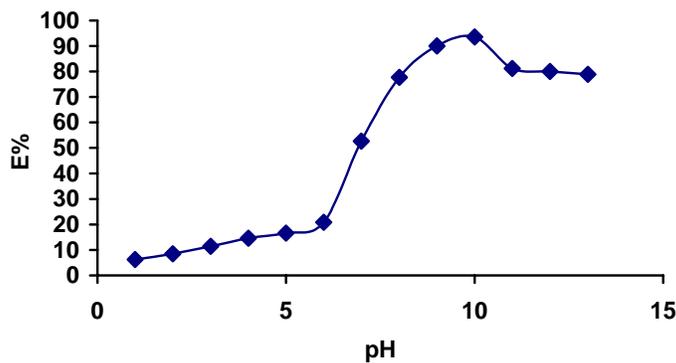
(II)

PDB18C6
(0.01) kd

$[(\text{M} \cdot \text{Lp}^+)_2 \cdot \text{Cu}(\text{OH})_4^{-2}]$

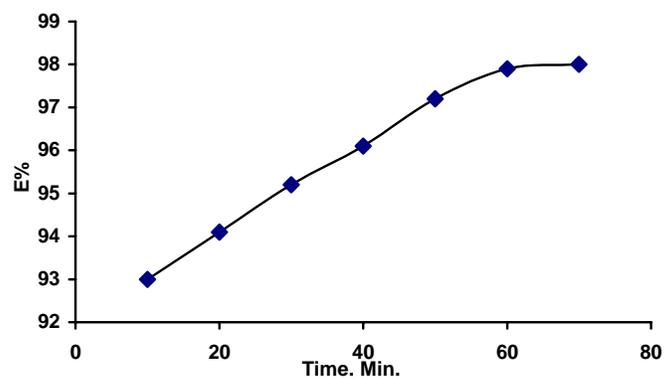
(12)

$[\text{H} \cdot \text{Lp}^+ \cdot \text{OH}^-]$



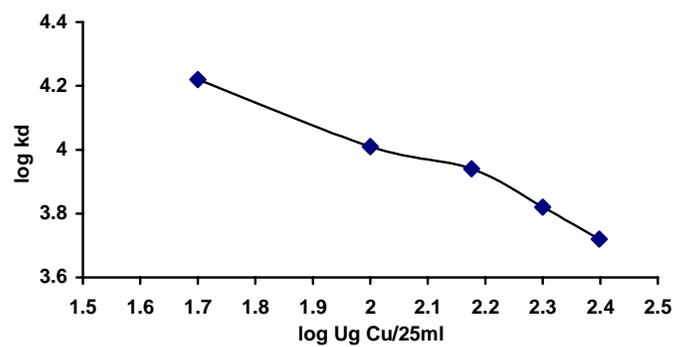
(II)

(2)



(II)

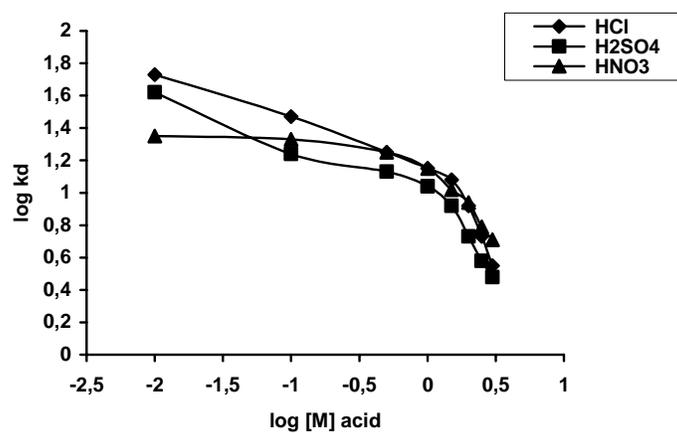
(3)



Kd

(II)

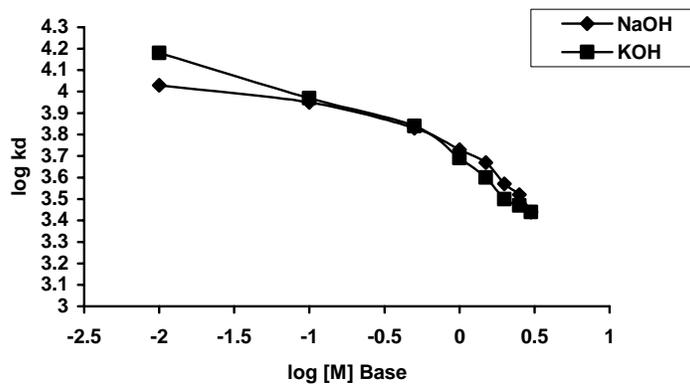
(4)



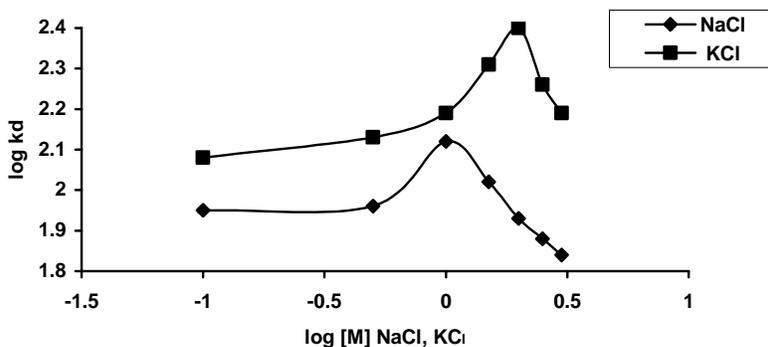
(II)

Kd

(5)



(II) Kd (6)



(II) Kd (7)

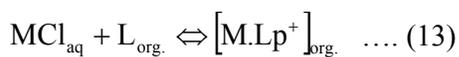
(1.00) (7)

(2.00-0.10)

(II)

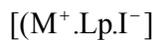
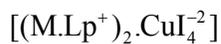
(KCl, NaCl)

[24] -0.10)



(0.10

.(K⁺, Na⁺) M⁺



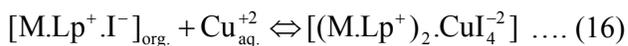
kd

(8)

:

-0.01)

(KI) (NaI)



(Cl⁻)

(I⁻)

(II)

(CuI₂)

[26]

[25]

$$Q = \frac{(C_0 - C_e)VL}{wt_{(g)} \text{ of crown ether}} \dots (17)$$

(10)

$$Q = \frac{kd \cdot VL \cdot C_e}{wt_{(g)} \cdot C_0} \dots (9)$$

(V/V 40%)

(activity)

[28]

kd

[21,29]

(0.1)

KOH (0.01) PDB18C6
(0.981mg/lg of PDB18C6)

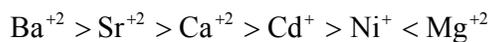


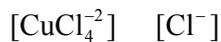
[30]

M⁺

m

(11)





(II)

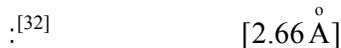
[31]

:



(12)

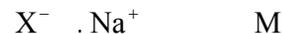
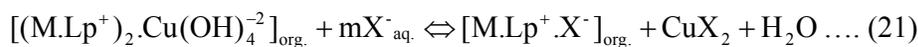
(II)



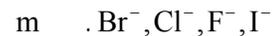
[24]

[32]

$$\frac{\text{I.D of Ions}}{\text{I.D of cavity}} = \frac{2.7 \overset{\circ}{\text{A}}}{2.66 \overset{\circ}{\text{A}}} = 0.9$$



[26]



$$\Delta\text{Hex} = (-9.2427)$$

$$\Delta\text{Gex} = (-21.819)\text{to}(-21.341)$$

$$\Delta\text{S}^\circ\text{ex} = (41.817)\text{to}(34.273)$$

$$(353\text{K}^\circ - 288\text{K}^\circ)$$

[33] (Vant-Hoff)

$$\log \text{Kex} = \frac{-\Delta\text{H}}{2.303\text{RT}} + \text{constant} \dots (22)$$

(1/T(K⁰))

(log Kex)

$$\frac{-\Delta\text{H}}{2.303\text{RT}}$$

(ΔHex)

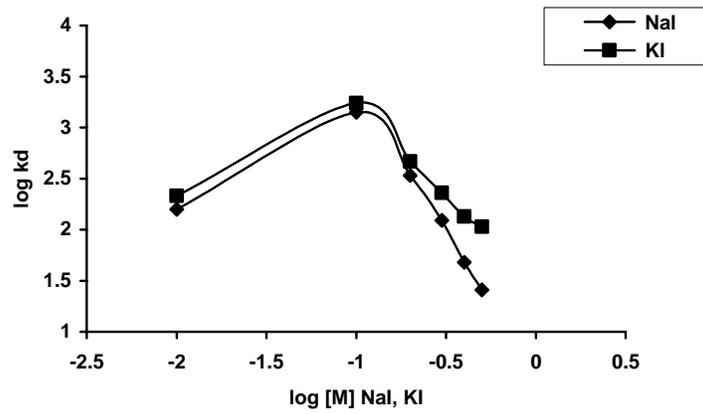
[34]

(13)

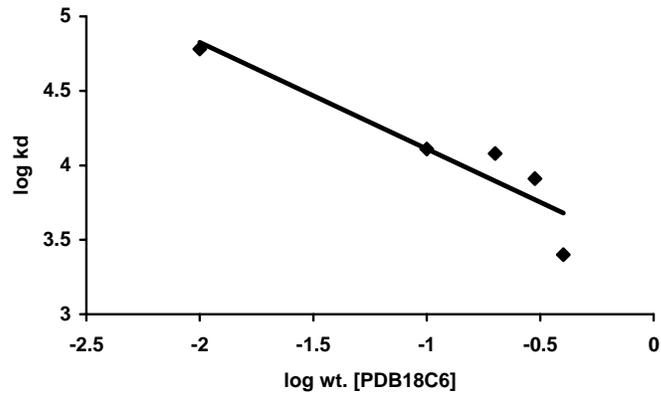
ΔHex

ΔGex

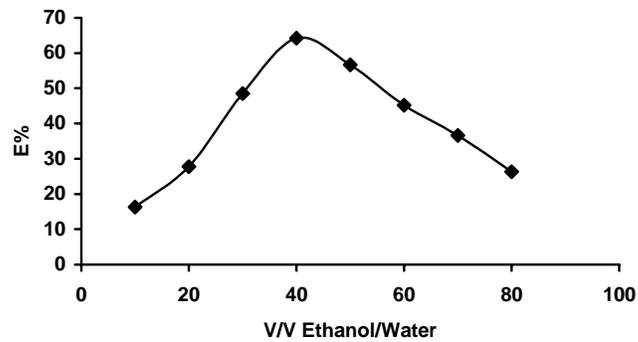
(Exothermic)



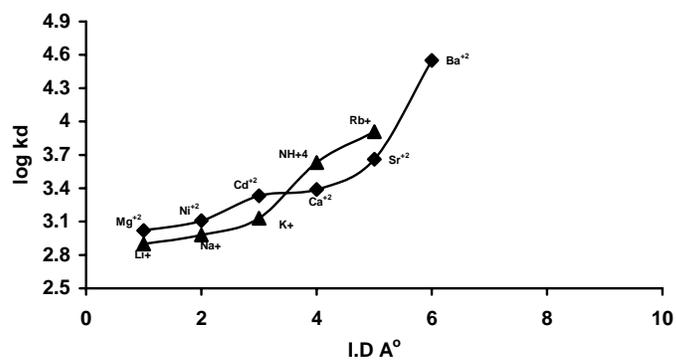
(II) Kd (KI) (NaI) (8)



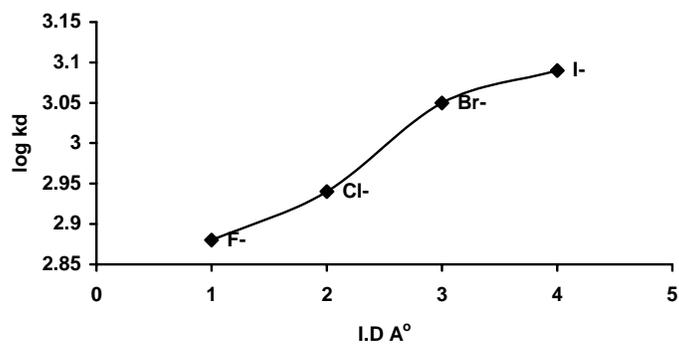
(II) kd (9)



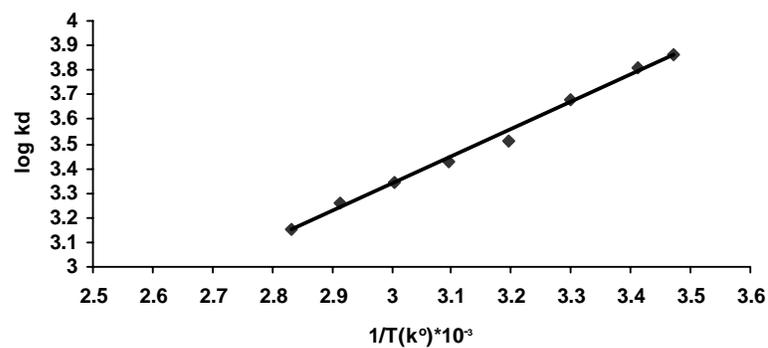
(II) $E\%$ (10)



(II) Kd (11)



(II) kd (12)



(II) kd (13)

Mobile Phase • (II)
 stepwise
 KOH (2.00) .1 (II)
 .Pd PDB18C6
 .Cu HCl (1.00) .2 (14)
 1ml/min Flow rate • (II)
 (14) .PDB18C6 resin

(1g swelled PDB18C6)

: (α)

$$\alpha = \frac{kd_{Pd}}{kd_{Cu}} \dots (23)$$

$$\alpha = \frac{19.5}{93.2} = 0.2$$

: (2) kd

(10ml)

(Elution Curve)

: (14)

kd_{Cu} kd_{Pd}
 Cu⁺ Pd²⁺

(2.00) KOH

V_{max} = 40ml C_{max} = 42.5µg Pd/15ml W/2 = 13ml L = 2cm

.Width of Elution Peak = W

.Effective Plate Number = N

.High of theoretical plate = H

. Length of Column = L

V_{max} = 15ml C_{max} = 43.5µgCu/25ml W/2 = 10ml L = 2cm

.[134]

(N)

$N = 5.54 \left[\frac{V_{max}}{W/2} \right]^2$	$N = 5.54 \left[\frac{V_{max}}{W/2} \right]^2$
$N_{Pd} = 5.54 \left[\frac{40}{13} \right]^2$	$N_{Cu} = 5.54 \left[\frac{15}{10} \right]^2$
$N_{Pd} = 52.45$	$N_{Cu} = 12.465$

$$H = L/N = \frac{2}{52.45} = 0.038\text{cm}$$

$$H = L/N = \frac{2}{12.465} = 0.16\text{cm}$$

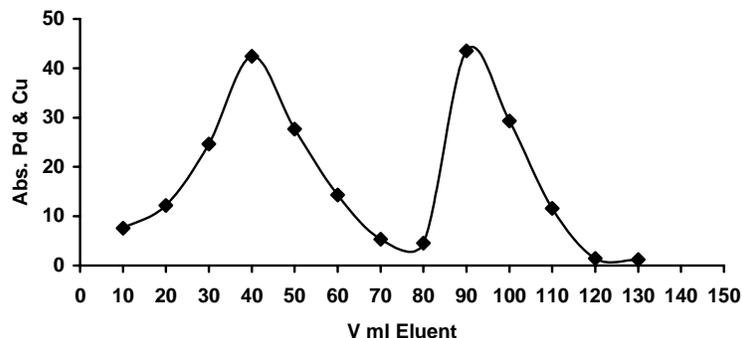
(II)

(14)

(II) ()

(2M KOH)

(80)



(PDB18C6

(II)

(II)

(14)

resin)

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